

Strong-Bolt® 2 Design Information — Concrete

Carbon-Steel Strong-Bolt 2 Installation Information¹

Characteristic	Symbol	Units	Nominal Anchor Diameter, d_a (in.)											
			$\frac{1}{4}$ ⁴	$\frac{3}{8}$ ⁵		$\frac{1}{2}$ ⁵		$\frac{5}{8}$ ⁵		$\frac{3}{4}$ ⁵		1 ⁵		
Installation Information														
Nominal Diameter	d_a	in.	$\frac{1}{4}$	$\frac{3}{8}$		$\frac{1}{2}$		$\frac{5}{8}$		$\frac{3}{4}$		1		
Drill Bit Diameter	d	in.	$\frac{1}{4}$	$\frac{3}{8}$		$\frac{1}{2}$		$\frac{5}{8}$		$\frac{3}{4}$		1		
Baseplate Clearance Hole Diameter ²	d_c	in.	$\frac{5}{16}$	$\frac{7}{16}$		$\frac{9}{16}$		$\frac{11}{16}$		$\frac{7}{8}$		$1\frac{1}{8}$		
Installation Torque	T_{inst}	ft-lbf	4	30		60		90		150		230		
Nominal Embedment Depth	h_{nom}	in.	$1\frac{3}{4}$	$1\frac{7}{8}$	$2\frac{7}{8}$	$2\frac{3}{4}$		$3\frac{7}{8}$	$3\frac{3}{8}$	$5\frac{1}{8}$	$4\frac{1}{8}$	$5\frac{3}{4}$	$5\frac{1}{4}$	$9\frac{3}{4}$
Effective Embedment Depth	h_{ef}	in.	$1\frac{1}{2}$	$1\frac{1}{2}$	$2\frac{1}{2}$	$2\frac{1}{4}$		$3\frac{3}{8}$	$2\frac{3}{4}$	$4\frac{1}{2}$	$3\frac{3}{8}$	5	$4\frac{1}{2}$	9
Minimum Hole Depth	h_{hole}	in.	$1\frac{7}{8}$	2	3	3		$4\frac{1}{8}$	$3\frac{5}{8}$	$5\frac{3}{8}$	$4\frac{3}{8}$	6	$5\frac{1}{2}$	10
Minimum Overall Anchor Length	ℓ_{anch}	in.	$2\frac{1}{4}$	$2\frac{3}{4}$	$3\frac{1}{2}$	$3\frac{3}{4}$		$5\frac{1}{2}$	$4\frac{1}{2}$	6	$5\frac{1}{2}$	7	7	13
Critical Edge Distance	c_{ac}	in.	$2\frac{1}{2}$	$6\frac{1}{2}$	6	$6\frac{1}{2}$	$6\frac{1}{2}$	$7\frac{1}{2}$	$7\frac{1}{2}$	9	9	8	18	$13\frac{1}{2}$
Minimum Edge Distance	c_{min}	in.	$1\frac{3}{4}$	6		7	4	4	$6\frac{1}{2}$		$6\frac{1}{2}$		8	
	for $s \geq$	in.	—	—		—	—	—	—		8		—	
Minimum Spacing	s_{min}	in.	$2\frac{1}{4}$	3		7	4	4	5		7		8	
	for $c \geq$	in.	—	—		—	—	—	—		8		—	
Minimum Concrete Thickness	h_{min}	in.	$3\frac{1}{4}$	$3\frac{1}{4}$	$4\frac{1}{2}$	$4\frac{1}{2}$	$5\frac{1}{2}$	6	$5\frac{1}{2}$	$7\frac{7}{8}$	$6\frac{3}{4}$	$8\frac{3}{4}$	8	$13\frac{1}{2}$
Additional Data														
Yield Strength	f_{ya}	psi	56,000	92,000		85,000				70,000		60,000		
Tensile Strength	f_{uta}	psi	70,000	115,000				110,000		78,000				
Minimum Tensile and Shear Stress Area	A_{se}	in. ²	0.0318	0.0514		0.105		0.166		0.270		0.472		
Axial Stiffness in Service Load Range — Cracked and Uncracked Concrete	β	lb./in.	73,700 ³	34,820		63,570		91,370		118,840		299,600		

1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D.

2. The clearance must comply with applicable code requirements for the connected element.

3. The tabulated value of β for $\frac{1}{4}$ "-diameter carbon steel Strong-Bolt 2 anchor is for installations in uncracked concrete only.

4. The $\frac{1}{4}$ "-diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in this table.

5. The $\frac{3}{8}$ "- through 1"-diameter (9.5mm through 25.4mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in this table.

* See p.13 for an explanation of the load table icons.

Strong-Bolt® 2 Design Information — Concrete

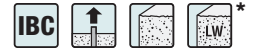
Stainless-Steel Strong-Bolt 2 Installation Information¹

Characteristic	Symbol	Units	Nominal Anchor Diameter, d_a (in.)									
			$\frac{1}{4}$ ⁴		$\frac{3}{8}$ ⁵		$\frac{1}{2}$ ⁵		$\frac{5}{8}$ ⁵		$\frac{3}{4}$ ⁵	
Installation Information												
Nominal Diameter	d_a	in.	$\frac{1}{4}$		$\frac{3}{8}$		$\frac{1}{2}$		$\frac{5}{8}$		$\frac{3}{4}$	
Drill Bit Diameter	d	in.	$\frac{1}{4}$		$\frac{3}{8}$		$\frac{1}{2}$		$\frac{5}{8}$		$\frac{3}{4}$	
Baseplate Clearance Hole Diameter ²	d_c	in.	$\frac{5}{16}$		$\frac{7}{16}$		$\frac{9}{16}$		$\frac{11}{16}$		$\frac{7}{8}$	
Installation Torque	T_{inst}	ft-lbf	4		30		65		80		150	
Nominal Embedment Depth	h_{nom}	in.	$1\frac{3}{4}$	$1\frac{7}{8}$	$2\frac{1}{8}$	$2\frac{3}{4}$	$3\frac{7}{8}$	$3\frac{3}{8}$	$5\frac{1}{8}$	$4\frac{1}{8}$	$5\frac{3}{4}$	
Effective Embedment Depth	h_{ef}	in.	$1\frac{1}{2}$	$1\frac{1}{2}$	$2\frac{1}{2}$	$2\frac{1}{4}$	$3\frac{3}{8}$	$2\frac{3}{4}$	$4\frac{1}{2}$	$3\frac{3}{8}$	5	
Minimum Hole Depth	h_{hole}	in.	$1\frac{7}{8}$	2	3	3	$4\frac{1}{8}$	$3\frac{3}{8}$	$5\frac{3}{8}$	$4\frac{3}{8}$	6	
Minimum Overall Anchor Length	ℓ_{anch}	in.	$2\frac{1}{4}$	$2\frac{3}{4}$	$3\frac{1}{2}$	$3\frac{3}{4}$	$5\frac{1}{2}$	$4\frac{1}{2}$	6	$5\frac{1}{2}$	7	
Critical Edge Distance	c_{ac}	in.	$2\frac{1}{2}$	$6\frac{1}{2}$	$8\frac{1}{2}$	$4\frac{1}{2}$	7	$7\frac{1}{2}$	9	8	8	
Minimum Edge Distance	c_{min}	in.	$1\frac{3}{4}$	6	$6\frac{1}{2}$	5	4	4	6			
	for $s \geq$	in.	—	10	—	—	8	8	—			
Minimum Spacing	s_{min}	in.	$2\frac{1}{4}$	3	8	$5\frac{1}{2}$	4	$6\frac{1}{4}$	$6\frac{1}{2}$			
	for $c \geq$	in.	—	10	—	—	8	$5\frac{1}{2}$	—			
Minimum Concrete Thickness	h_{min}	in.	$3\frac{1}{4}$	$3\frac{1}{4}$	$4\frac{1}{2}$	$4\frac{1}{2}$	6	$5\frac{1}{2}$	$7\frac{7}{8}$	$6\frac{3}{4}$	$8\frac{3}{4}$	
Additional Data												
Yield Strength	f_{ya}	psi	96,000		80,000		92,000		82,000		68,000	
Tensile Strength	f_{uta}	psi	120,000		100,000		115,000		108,000		95,000	
Minimum Tensile and Shear Stress Area	A_{se}	in. ²	0.0255		0.0514		0.105		0.166		0.270	
Axial Stiffness in Service Load Range — Cracked and Uncracked Concrete	β	lb./in.	54,430 ³		29,150		54,900		61,270		154,290	

- The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D.
- The clearance must comply with applicable code requirements for the connected element.
- The tabulated value of β for $\frac{1}{4}$ "-diameter stainless-steel Strong-Bolt 2 anchor is for installations in uncracked concrete only.
- The $\frac{1}{4}$ "-diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in this table.
- The $\frac{3}{8}$ "- through $\frac{3}{4}$ "-diameter (9.5mm through 19.1mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in this table.

* See p. 13 for an explanation of the load table icons.

Strong-Bolt® 2 Design Information — Concrete



Carbon-Steel Strong-Bolt 2 Tension Strength Design Data¹

Characteristic	Symbol	Units	Nominal Anchor Diameter, d_a (in.)												
			$\frac{1}{4}^8$	$\frac{3}{8}^9$	$\frac{1}{2}^9$	$\frac{5}{8}^9$	$\frac{3}{4}^9$	1^9							
Anchor Category	1, 2 or 3	—	1									2			
Nominal Embedment Depth	h_{nom}	in.	1¾	1⅞	2⅞	2¾	3⅞	3¾	5⅞	4⅞	5¾	5¼	9¼		
Steel Strength in Tension (ACI 318 Section D.5.1)															
Steel Strength in Tension	N_{sa}	lb.	2,225	5,600	12,100	19,070	29,700						36,815		
Strength Reduction Factor — Steel Failure ²	ϕ_{sa}	—	0.75									0.65			
Concrete Breakout Strength in Tension (ACI 318 Section D.5.2)¹⁰															
Effective Embedment Depth	h_{ef}	in.	1½	1½	2½	2¼	3¾	2¾	4½	3¾	5	4½	9		
Critical Edge Distance	c_{ac}	in.	2½	6½	6	6½	7½	7½	9	9	8	18	13½		
Effectiveness Factor — Uncracked Concrete	k_{uncr}	—	24												
Effectiveness Factor — Cracked Concrete	k_{cr}	—	— ⁷					17							
Modification Factor	$\psi_{c,N}$	—	— ⁷					1.00							
Strength Reduction Factor — Concrete Breakout Failure ³	ϕ_{cb}	—	0.65									0.55			
Pullout Strength in Tension (ACI 318 Section D.5.3)¹⁰															
Pullout Strength, Cracked Concrete ($f'_c = 2,500$ psi)	$N_{p,cr}$	lb.	— ⁷	1,300 ⁵	2,775 ⁵	N/A ⁴	3,735 ⁵	N/A ⁴	6,985 ⁵	N/A ⁴	8,500 ⁵	7,700 ⁵	11,185 ⁵		
Pullout Strength, Uncracked Concrete ($f'_c = 2,500$ psi)	$N_{p,uncr}$	lb.	N/A ⁴	N/A ⁴	3,340 ⁵	3,615 ⁵	5,255 ⁵	N/A ⁴	9,025 ⁵	7,115 ⁵	8,870 ⁵	8,360 ⁵	9,690 ⁵		
Strength Reduction Factor — Pullout Failure ⁶	ϕ_p	—	0.65									0.55			
Tensile Strength for Seismic Applications (ACI 318 Section D.3.3.)¹⁰															
Tension Strength of Single Anchor for Seismic Loads ($f'_c = 2,500$ psi)	$N_{p,eq}$	lb.	— ⁷	1,300 ⁵	2,775 ⁵	N/A ⁴	3,735 ⁵	N/A ⁴	6,985 ⁵	N/A ⁴	8,500 ⁵	7,700 ⁵	11,185 ⁵		
Strength Reduction Factor — Pullout Failure ⁶	ϕ_{eq}	—	0.65									0.55			

- The information presented in this table must be used in conjunction with the design criteria of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, as applicable, except as modified below.
- The tabulated value of ϕ_{sa} applies when the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ_{sa} must be determined in accordance with ACI 318-11 D.4.4.
- The tabulated value of ϕ_{cb} applies when both the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition B are met. Condition B applies where supplementary reinforcement is not provided. For installations where complying supplementary reinforcement can be verified, the ϕ_{cb} factors described in ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition A are allowed. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ_{cb} must be determined in accordance with ACI 318-11 D.4.4(c).
- N/A (not applicable) denotes that pullout resistance does not need to be considered.
- The characteristic pullout strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by $(f'_c/2,500 \text{ psi})^{0.5}$.
- The tabulated value of ϕ_p or ϕ_{eq} applies when the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition B are met. If the load combinations of ACI 318-11 Appendix C are used, appropriate value of ϕ must be determined in accordance with ACI 318-11 Section D.4.4(c).
- The $\frac{1}{4}$ "-diameter carbon steel Strong-Bolt 2 anchor installation in cracked concrete is beyond the scope of this table.
- The $\frac{1}{4}$ "-diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on p. 136.
- The $\frac{3}{8}$ "- through $\frac{3}{4}$ "-diameter (9.5mm through 25.4mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on p. 136.

* See p. 13 for an explanation of the load table icons.

Strong-Bolt® 2 Design Information — Concrete

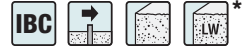
Stainless-Steel Strong-Bolt 2 Tension Strength Design Data¹

Characteristic	Symbol	Units	Nominal Anchor Diameter, d_a (in.)								
			¼"	⅜"	½"	⅝"	¾"	1"	1 ¼"	1 ½"	2"
Anchor Category	1, 2 or 3	—	1								
Nominal Embedment Depth	h_{nom}	in.	1 ¾	1 ⅞	2 ⅞	2 ¾	3 ⅞	3 ¾	5 ⅞	4 ⅞	5 ¾
Steel Strength in Tension (ACI 318 Section D.5.1)											
Steel Strength in Tension	N_{sa}	lb.	3,060	5,140	12,075	17,930	25,650				
Strength Reduction Factor — Steel Failure ²	ϕ_{sa}	—	0.75								
Concrete Breakout Strength in Tension (ACI 318 Section D.5.2)¹²											
Effective Embedment Depth	h_{ef}	in.	1 ½	1 ½	2 ½	2 ¼	3 ⅞	2 ¾	4 ½	3 ⅞	5
Critical Edge Distance	c_{ac}	in.	2 ½	6 ½	8 ½	4 ½	7	7 ½	9	8	8
Effectiveness Factor — Uncracked Concrete	k_{uncr}	—	24								
Effectiveness Factor — Cracked Concrete	k_{cr}	—	17								
Modification Factor	$\psi_{c,N}$	—	1.00								
Strength Reduction Factor — Concrete Breakout Failure ³	ϕ_{cb}	—	0.65								
Pullout Strength in Tension (ACI 318 Section D.5.3)¹²											
Pullout Strength, Cracked Concrete ($f'_c = 2,500$ psi)	$N_{p,cr}$	lb.	— ⁹	1,720 ⁶	3,145 ⁶	2,560 ⁵	4,305 ⁵	N/A ⁴	6,545 ⁷	N/A ⁴	8,230 ⁵
Pullout Strength, Uncracked Concrete ($f'_c = 2,500$ psi)	$N_{p,uncr}$	lb.	1,925 ⁷	N/A ⁴	4,770 ⁶	3,230 ⁵	4,495 ⁵	N/A ⁴	7,615 ⁵	7,725 ⁷	9,625 ⁷
Strength Reduction Factor — Pullout Failure ⁸	ϕ_p	—	0.65								
Tensile Strength for Seismic Applications (ACI 318 Section D.3.3.)¹²											
Tension Strength of Single Anchor for Seismic Loads ($f'_c = 2,500$ psi)	$N_{p,eq}$	lb.	— ⁹	1,720 ⁶	2,830 ⁶	2,560 ⁵	4,305 ⁵	N/A ⁴	6,545 ⁷	N/A ⁴	8,230 ⁵
Strength Reduction Factor — Pullout Failure ⁸	ϕ_{eq}	—	0.65								

- The information presented in this table must be used in conjunction with the design criteria of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, as applicable, except as modified below.
- The tabulated value of ϕ_{sa} applies when the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ_{sa} must be determined in accordance with ACI 318-11 D.4.4.
- The tabulated value of ϕ_{cb} applies when both the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition B are met. Condition B applies where supplementary reinforcement is not provided. For installations where complying supplementary reinforcement can be verified, the ϕ_{cb} factors described in ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition A are allowed. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ_{cb} must be determined in accordance with ACI 318-11 D.4.4(c).
- N/A (not applicable) denotes that pullout resistance does not need to be considered.
- The characteristic pullout strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by $(f'_c/2,500 \text{ psi})^{0.5}$.
- The characteristic pullout strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by $(f'_c/2,500 \text{ psi})^{0.3}$.
- The characteristic pullout strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by $(f'_c/2,500 \text{ psi})^{0.4}$.
- The tabulated value of ϕ_p or ϕ_{eq} applies when the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition B are met. If the load combinations of ACI 318-11 Appendix C are used, appropriate value of ϕ must be determined in accordance with ACI 318-11 Section D.4.4(c).
- The ¼"-diameter stainless-steel Strong-Bolt 2 anchor installation in cracked concrete is beyond the scope of this table.
- The ¼"-diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on p. 136.
- The ⅜"- through ¾"-diameter (9.5mm through 19.1mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on p. 136.

* See p. 13 for an explanation of the load table icons.

Strong-Bolt® 2 Design Information — Concrete

Carbon-Steel Strong-Bolt 2 Shear Strength Design Data¹

Characteristic	Symbol	Units	Nominal Anchor Diameter, d_a (in.)										
			$\frac{1}{4}^6$	$\frac{3}{8}^7$	$\frac{1}{2}^7$	$\frac{5}{8}^7$	$\frac{3}{4}^7$	1^7					
Anchor Category	1, 2 or 3	—	1									2	
Nominal Embedment Depth	h_{nom}	in.	1 $\frac{3}{4}$	1 $\frac{7}{8}$	2 $\frac{7}{8}$	2 $\frac{3}{4}$	3 $\frac{7}{8}$	3 $\frac{3}{8}$	5 $\frac{1}{8}$	4 $\frac{1}{8}$	5 $\frac{3}{4}$	5 $\frac{1}{4}$	9 $\frac{3}{4}$
Steel Strength in Shear (ACI 318 Section D.6.1)													
Steel Strength in Shear	V_{sa}	lb.	965	1,800	7,235	11,035	14,480	15,020					
Strength Reduction Factor — Steel Failure ²	ϕ_{sa}	—	0.65									0.60	
Concrete Breakout Strength in Shear (ACI 318 Section D.6.2)⁸													
Outside Diameter	d_a	in.	0.25	0.375	0.500	0.625	0.750	1.00					
Load-Bearing Length of Anchor in Shear	ℓ_e	in.	1.500	1.500	2.500	2.250	3.375	2.750	4.500	3.375	5.000	4.500	8.000
Strength Reduction Factor — Concrete Breakout Failure ²	ϕ_{cb}	—	0.70										
Concrete Pryout Strength in Shear (ACI 318 Section D.6.3)													
Coefficient for Pryout Strength	k_{cp}	—	1.0	2.0	1.0	2.0							
Effective Embedment Depth	h_{ef}	in.	1 $\frac{1}{2}$	1 $\frac{1}{2}$	2 $\frac{1}{2}$	2 $\frac{1}{4}$	3 $\frac{3}{8}$	2 $\frac{3}{4}$	4 $\frac{1}{2}$	3 $\frac{3}{8}$	5	4 $\frac{1}{2}$	9
Strength Reduction Factor — Concrete Pryout Failure ⁴	ϕ_{cp}	—	0.70										
Steel Strength in Shear for Seismic Applications (ACI 318 Section D.3.3.)													
Shear Strength of Single Anchor for Seismic Loads ($f'_c = 2,500$ psi)	$V_{sa,eq}$	lb.	— ⁵	1,800	6,510	9,930	11,775	15,020					
Strength Reduction Factor — Steel Failure ²	ϕ_{sa}	—	0.65									0.60	

- The information presented in this table must be used in conjunction with the design criteria of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, except as modified below.
- The tabulated value of ϕ_{sa} applies when the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ_{sa} must be determined in accordance with ACI 318 D.4.4.
- The tabulated value of ϕ_{cb} applies when both the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition B are met. Condition B applies where supplementary reinforcement is not provided. For installations where complying supplementary reinforcement can be verified, the ϕ_{cb} factors described in ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition A are allowed. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ_{cb} must be determined in accordance with ACI 318-11 D.4.4(c).
- The tabulated value of ϕ_{cp} applies when both the load combinations of IBC Section 1605.2, ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition B are met. If the load combinations of ACI 318-11 Appendix C are used, appropriate value of ϕ_{cp} must be determined in accordance with ACI 318-11 Section D.4.4(c).
- The $\frac{1}{4}$ "-diameter carbon steel Strong-Bolt 2 anchor installation in cracked concrete is beyond the scope of this table.
- The $\frac{1}{4}$ "-diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on p. 136.
- The $\frac{3}{8}$ "- through 1"-diameter (9.5mm through 25.4mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flute meets the minimum thickness specified in the table on p. 136.

* See p. 13 for an explanation of the load table icons.

Strong-Bolt® 2 Design Information — Concrete

Stainless-Steel Strong-Bolt 2 Shear Strength Design Data¹

Characteristic	Symbol	Units	Nominal Anchor Diameter, d_a (in.)								
			$\frac{1}{4}^6$	$\frac{3}{8}^7$	$\frac{1}{2}^7$	$\frac{5}{8}^7$	$\frac{3}{4}^7$				
Anchor Category	1, 2 or 3	—	1								
Nominal Embedment Depth	h_{nom}	in.	$1\frac{3}{4}$	$1\frac{7}{8}$	$2\frac{7}{8}$	$2\frac{3}{4}$	$3\frac{7}{8}$	$3\frac{3}{8}$	$5\frac{1}{8}$	$4\frac{1}{8}$	$5\frac{3}{4}$
Steel Strength in Shear (ACI 318 Section D.6.1)											
Steel Strength in Shear	V_{sa}	lb.	1,605	3,085	7,245	6,745	10,760	15,045			
Strength Reduction Factor — Steel Failure ²	ϕ_{sa}	—	0.65								
Concrete Breakout Strength in Shear (ACI 318 Section D.6.2)⁸											
Outside Diameter	d_a	in.	0.250	0.375	0.500	0.625	0.750				
Load Bearing Length of Anchor in Shear	ℓ_e	in.	1.500	1.500	2.500	2.250	3.375	2.750	4.500	3.375	5.000
Strength Reduction Factor — Concrete Breakout Failure ³	ϕ_{cb}	—	0.70								
Concrete Pryout Strength in Shear (ACI 318 Section D.6.3)											
Coefficient for Pryout Strength	k_{cp}	—	1.0	2.0	1.0	2.0					
Effective Embedment Depth	h_{ef}	in.	$1\frac{1}{2}$	$1\frac{1}{2}$	$2\frac{1}{2}$	$2\frac{1}{4}$	$3\frac{3}{8}$	$2\frac{3}{4}$	$4\frac{1}{2}$	$3\frac{3}{8}$	5
Strength Reduction Factor — Concrete Pryout Failure ⁴	ϕ_{cp}	—	0.70								
Steel Strength in Shear for Seismic Applications (ACI 318 Section D.3.3.)											
Shear Strength of Single Anchor for Seismic Loads ($f'_c = 2,500$ psi)	$V_{sa,eq}$	lb.	— ⁵	3,085	6,100	6,745	10,760	13,620			
Strength Reduction Factor — Steel Failure ²	ϕ_{sa}	—	0.65								

- The information presented in this table must be used in conjunction with the design criteria of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, except as modified below.
- The tabulated value of ϕ_{sa} applies when the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ_{sa} must be determined in accordance with ACI 318 D.4.4.
- The tabulated value of ϕ_{cb} applies when both the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition B are met. Condition B applies where supplementary reinforcement is not provided. For installations where complying supplementary reinforcement can be verified, the ϕ_{cb} factors described in ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition A are allowed. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ_{cb} must be determined in accordance with ACI 318-11 D.4.4(c).
- The tabulated value of ϕ_{cp} applies when both the load combinations of IBC Section 1605.2, ACI 318-14 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition B are met. If the load combinations of ACI 318-11 Appendix C are used, appropriate value of ϕ_{cp} must be determined in accordance with ACI 318-11 Section D.4.4(c).
- The $\frac{1}{4}$ "-diameter stainless-steel Strong-Bolt 2 anchor installation in cracked concrete is beyond the scope of this table.
- The $\frac{1}{4}$ "-diameter (6.4mm) anchor may be installed in top of uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flange meets the minimum thickness specified in the table on p. 136.
- The $\frac{3}{8}$ "- through $\frac{3}{4}$ "-diameter (9.5mm through 19.1mm) anchors may be installed in top of cracked and uncracked normal-weight and sand-lightweight concrete over profile steel deck, where concrete thickness above upper flange meets the minimum thickness specified in the table on p. 136.

* See p. 13 for an explanation of the load table icons.

Strong-Bolt® 2 Design Information — Concrete

Carbon-Steel Strong-Bolt 2 Information for Installation in the Topside of Concrete-Filled Profile Steel Deck Floor and Roof Assemblies^{1,2,3,4}



Design Information	Symbol	Units	Nominal Anchor Diameter (in.)		
			3/8	1/2	5/8
Nominal Embedment Depth	h_{nom}	in.	1 7/8	2 3/4	3 1/2
Effective Embedment Depth	h_{ef}	in.	1 1/2	2 1/4	3 1/4
Minimum Concrete Thickness ⁵	$h_{min,deck}$	in.	2 1/2	3 1/4	3 1/4
Critical Edge Distance	$C_{ac,deck,top}$	in.	4 3/4	4	4
Minimum Edge Distance	$C_{min,deck,top}$	in.	4 3/4	4 1/2	4 3/4
Minimum Spacing	$S_{min,deck,top}$	in.	7	6 1/2	8

For SI: 1 inch = 25.4mm; 1 lbf = 4.45N

1. Installation must comply with the table on p. 136 and Figure 1 below.
2. Design capacity shall be based on calculations according to values in the tables on pp. 138 and 140.
3. Minimum flute depth (distance from top of flute to bottom of flute) is 1 1/2".
4. Steel deck thickness shall be a minimum 20 gauge.
5. Minimum concrete thickness ($h_{min,deck}$) refers to concrete thickness above upper flute.

Stainless-Steel Strong-Bolt 2 Information for Installation in the Topside of Concrete-Filled Profile Steel Deck Floor and Roof Assemblies^{1,2,3,4}



Design Information	Symbol	Units	Nominal Anchor Diameter (in.)		
			3/8	1/2	5/8
Nominal Embedment Depth	h_{nom}	in.	1 7/8	2 3/4	3 1/2
Effective Embedment Depth	h_{ef}	in.	1 1/2	2 1/4	3 1/4
Minimum Concrete Thickness ⁵	$h_{min,deck}$	in.	2 1/2	3 1/4	3 1/4
Critical Edge Distance	$C_{ac,deck,top}$	in.	4 3/4	4	4
Minimum Edge Distance	$C_{min,deck,top}$	in.	4 3/4	6	6
Minimum Spacing	$S_{min,deck,top}$	in.	6 1/2	8	8

For SI: 1 inch = 25.4mm; 1 lbf = 4.45N

1. Installation must comply with the table on p. 137 and Figure 1 below.
2. Design capacity shall be based on calculations according to values in the tables on pp. 139 and 141.
3. Minimum flute depth (distance from top of flute to bottom of flute) is 1 1/2".
4. Steel deck thickness shall be a minimum 20 gauge.
5. Minimum concrete thickness ($h_{min,deck}$) refers to concrete thickness above upper flute.

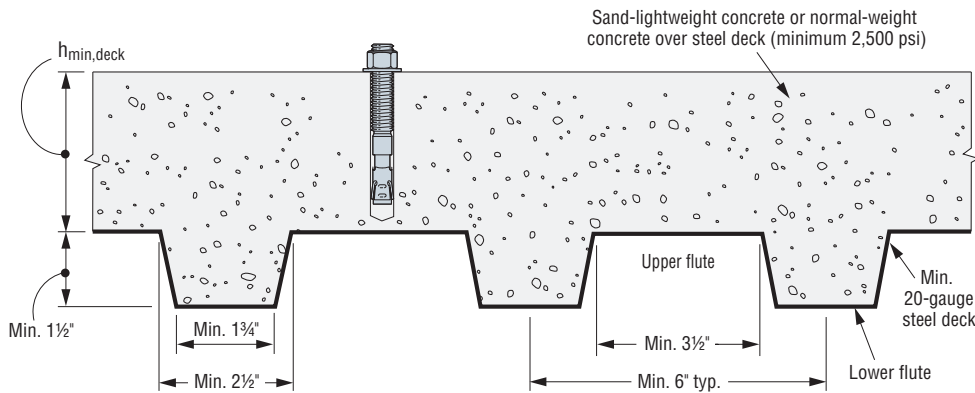


Figure 1

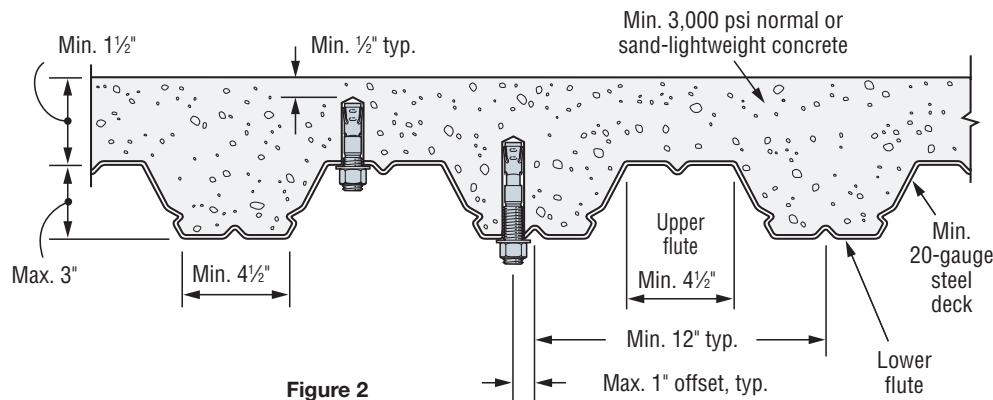


Figure 2

* See p. 13 for an explanation of the load table icons.

Strong-Bolt® 2 Design Information — Concrete

Carbon-Steel Strong-Bolt 2 Tension and Shear Strength Design Data for the Soffit of Concrete over Profile Steel Deck Floor and Roof Assemblies^{1,2,6,8,9}



Characteristic	Symbol	Units	Nominal Anchor Diameter (in.)								
			Carbon Steel								
			Lower Flute						Upper Flute		
			3/8	1/2	5/8	3/4	3/8	1/2			
Nominal Embedment Depth	h_{nom}	in.	2	3	2 3/4	4 1/2	3 3/8	5 1/8	4 1/8	2	2 3/4
Effective Embedment Depth	h_{ef}	in.	1 5/8	3	2 1/4	4	2 3/4	5	3 3/8	1 5/8	2 1/4
Installation Torque	T_{inst}	ft.-lbf.	30		60		90		150	30	60
Pullout Strength, concrete on metal deck (cracked) ^{3,4}	$N_{p,deck,cr}$	lb.	1,040 ⁷	2,615 ⁷	2,040 ⁷	2,730 ⁷	2,615 ⁷	4,990 ⁷	2,815 ⁷	1,340 ⁷	3,785 ⁷
Pullout Strength, concrete on metal deck (uncracked) ^{3,4}	$N_{p,deck,uncr}$	lb.	1,765 ⁷	3,150 ⁷	2,580 ⁷	3,840 ⁷	3,685 ⁷	6,565 ⁷	3,800 ⁷	2,275 ⁷	4,795 ⁷
Pullout Strength, concrete on metal deck (seismic) ^{3,4}	$N_{p,deck,eq}$	lb.	1,040 ⁷	2,615 ⁷	2,040 ⁷	2,730 ⁷	2,615 ⁷	4,990 ⁷	2,815 ⁷	1,340 ⁷	3,785 ⁷
Steel Strength in Shear, concrete on metal deck ⁵	$V_{sa,deck}$	lb.	1,595	3,490	2,135	4,580	2,640	7,000	4,535	3,545	5,920
Steel Strength in Shear, concrete on metal deck (seismic) ⁵	$V_{sa,deck,eq}$	lb.	1,595	3,490	1,920	4,120	2,375	6,300	3,690	3,545	5,330

- The information presented in this table must be used in conjunction with the design criteria of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, except as modified below.
- Profile steel deck must comply with the configuration in Figure 2 on the previous page, and have a minimum base-steel thickness of 0.035 inch (20 gauge). Steel must comply with ASTM A 653/A 653M SS Grade 33 with minimum yield strength of 33,000 psi. Concrete compressive strength shall be 3,000 psi minimum.
- For anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies, calculation of the concrete breakout strength may be omitted.
- In accordance with ACI 318-14 Section 17.4.3.2 or ACI 318-11 Section D.5.3.2, the nominal pullout strength in cracked concrete for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies $N_{p,deck,cr}$ shall be substituted for $N_{p,cr}$. Where analysis indicates no cracking at service loads, the normal pullout strength in uncracked concrete $N_{p,deck,uncr}$ shall be substituted for $N_{p,uncr}$. For seismic loads, $N_{p,deck,eq}$ shall be substituted for N_p .
- In accordance with ACI 318-14 Section 17.5.1.2(C) or ACI 318-11 Section D.6.1.2(c), the shear strength for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies $V_{sa,deck}$ shall be substituted for V_{sa} . For seismic loads, $V_{sa,deck,eq}$ shall be substituted for V_{sa} .
- The minimum anchor spacing along the flute must be the greater of $3.0h_{ef}$ or 1.5 times the flute width.
- The characteristic pull-out strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by $(f'_c / 3,000 \text{ psi})^{0.5}$.
- Concrete shall be normal-weight or structural sand-lightweight concrete having a minimum specified compressive strength, f'_c , of 3,000 psi.
- Minimum distance to edge of panel is $2h_{ef}$.

Stainless-Steel Strong-Bolt 2 Tension and Shear Strength Design Data for the Soffit of Concrete over Profile Steel Deck Floor and Roof Assemblies^{1,2,6,10,11}



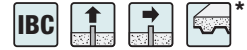
Characteristic	Symbol	Units	Stainless Steel								
			Lower Flute								
			Lower Flute						Upper Flute		
			3/8	1/2	5/8	3/4	3/8	1/2			
Nominal Embedment Depth	h_{nom}	in.	2	3 3/8	2 3/4	4 1/2	3 3/8	5 1/8	4 1/8	2	2 3/4
Effective Embedment Depth	h_{ef}	in.	1 5/8	3	2 1/4	4	2 3/4	5	3 3/8	1 5/8	2 1/4
Installation Torque	T_{inst}	ft.-lbf.	30		65		80		150	30	65
Pullout Strength, concrete on metal deck (cracked) ³	$N_{p,deck,cr}$	lb.	1,230 ⁸	2,605 ⁸	1,990 ⁷	2,550 ⁷	1,750 ⁹	4,020 ⁹	3,030 ⁷	1,550 ⁸	2,055 ⁷
Pullout Strength, concrete on metal deck (uncracked) ³	$N_{p,deck,uncr}$	lb.	1,580 ⁸	3,950 ⁸	2,475 ⁷	2,660 ⁷	2,470 ⁷	5,000 ⁷	4,275 ⁹	1,990 ⁸	2,560 ⁷
Pullout Strength, concrete on metal deck (seismic) ⁵	$N_{p,deck,eq}$	lb.	1,230 ⁸	2,345 ⁸	1,990 ⁷	2,550 ⁷	1,750 ⁹	4,020 ⁹	3,030 ⁷	1,550 ⁸	2,055 ⁷
Steel Strength in Shear, concrete on metal deck ⁴	$V_{sa,deck}$	lb.	2,285	3,085	3,430	4,680	3,235	5,430	6,135	3,085	5,955
Steel Strength in Shear, concrete on metal deck (seismic) ⁵	$V_{sa,deck,eq}$	lb.	2,285	3,085	2,400	3,275	3,235	5,430	5,520	3,085	4,170

- The information presented in this table must be used in conjunction with the design criteria of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, except as modified below.
- Profile steel deck must comply with the configuration in Figure 2 on the previous page, and have a minimum base-steel thickness of 0.035 inch (20 gauge). Steel must comply with ASTM A 653/A 653M SS Grade 33 with minimum yield strength of 33,000 psi. Concrete compressive strength shall be 3,000 psi minimum.
- For anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies, calculation of the concrete breakout strength may be omitted.
- In accordance with ACI 318-14 Section 17.4.3.2 or ACI 318-11 Section D.5.3.2, the nominal pullout strength in cracked concrete for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies $N_{p,deck,cr}$ shall be substituted for $N_{p,cr}$. Where analysis indicates no cracking at service loads, the normal pullout strength in uncracked concrete $N_{p,deck,uncr}$ shall be substituted for $N_{p,uncr}$. For seismic loads, $N_{p,deck,eq}$ shall be substituted for N_p .
- In accordance with ACI 318-14 Section 17.5.1.2(C) or ACI 318-11 Section D.6.1.2(c), the shear strength for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies $V_{sa,deck}$ shall be substituted for V_{sa} . For seismic loads, $V_{sa,deck,eq}$ shall be substituted for V_{sa} .
- The minimum anchor spacing along the flute must be the greater of $3.0h_{ef}$ or 1.5 times the flute width.
- The characteristic pull-out strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by $(f'_c / 3,000 \text{ psi})^{0.5}$.
- The characteristic pull-out strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by $(f'_c / 3,000 \text{ psi})^{0.3}$.
- The characteristic pull-out strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by $(f'_c / 3,000 \text{ psi})^{0.4}$.
- Concrete shall be normal-weight or structural sand-lightweight concrete having a minimum specified compressive strength, f'_c , of 3,000 psi.
- Minimum distance to edge of panel is $2h_{ef}$.

* See p. 13 for an explanation of the load table icons.

Strong-Bolt® 2 Design Information — Concrete

Carbon-Steel Strong-Bolt 2 Anchor Tension and Shear Strength Design Data for the Soffit of Concrete over Profile Steel Deck, Floor and Roof Assemblies^{1,2,6,8,9}



Mechanical Anchors

Characteristic	Symbol	Units	Carbon Steel Nominal Anchor Diameter (in.)					
			Installed in Lower Flute					
			3/8	1/2	5/8	3/4	1	1 1/8
Nominal Embedment Depth	h_{nom}	in.	2	3 3/8	2 3/4	4 1/2	3 3/8	5 5/8
Effective Embedment Depth	h_{ef}	in.	1 5/8	3	2 1/4	4	2 3/4	5
Minimum Hole Depth	h_{hole}	in.	2 1/8	3 1/2	3	4 3/4	3 5/8	5 5/8
Minimum Concrete Thickness	$h_{min,deck}$	in.	2	2	2	3 1/4	2	3 1/4
Installation Torque	T_{inst}	ft.-lbf.	30		60		90	
Pullout Strength, concrete on metal deck (cracked) ^{3,4,7}	$N_{p,deck,cr}$	lb.	1,295	2,705	2,585	4,385	3,015	5,120
Pullout Strength, concrete on metal deck (uncracked) ^{3,4,7}	$N_{p,deck,uncr}$	lb.	2,195	3,260	3,270	6,165	4,250	6,735
Pullout Strength, concrete on metal deck (seismic) ^{3,4,7}	$N_{p,deck,eq}$	lb.	1,295	2,705	2,585	4,385	3,015	5,120
Steel Strength in Shear, concrete on metal deck ⁵	$V_{sa,deck}$	lb.	1,535	3,420	2,785	5,950	3,395	6,745
Steel Strength in Shear, concrete on metal deck (seismic) ⁵	$V_{sa,deck,eq}$	lb.	1,535	3,420	2,505	5,350	3,055	6,070

- The information presented in this table must be used in conjunction with the design criteria of ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, except as modified below.
- Profile steel deck must comply with the configuration in Figure 3 below, and have a minimum base-steel thickness of 0.035 inch (20 gauge). Steel must comply with ASTM A 653/A 653M SS Grade 50 with minimum yield strength of 50,000 psi. Concrete compressive strength shall be 3,000 psi minimum.
- For anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies, calculation of the concrete breakout strength may be omitted.
- In accordance with ACI 318-14 Section 17.4.3.2 or ACI 318-11 Section D.5.3.2, the nominal pullout strength in cracked concrete for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies $N_{p,deck,cr}$ shall be substituted for $N_{p,cr}$. Where analysis indicates no cracking at service loads, the normal pullout strength in uncracked concrete $N_{p,deck,uncr}$ shall be substituted for $N_{p,uncr}$. For seismic loads, $N_{p,deck,eq}$ shall be substituted for $N_{p,cr}$.
- In accordance with ACI 318-14 Section 17.5.1.2(c) or ACI 318-11, the shear strength for anchors installed in the soffit of sand-lightweight or normal-weight concrete over metal deck floor and roof assemblies $V_{sa,deck}$ shall be substituted for V_{sa} . For seismic loads, $V_{sa,deck,eq}$ shall be substituted for V_{sa} .
- The minimum anchor spacing along the flute must be the greater of $3.0h_{ef}$ or 1.5 times the flute width.
- The characteristic pull-out strength for greater concrete compressive strengths shall be increased by multiplying the tabular value by $(f'_c / 3,000 \text{ psi})^{0.5}$.
- Concrete shall be normal-weight or structural sand-lightweight concrete having a minimum specified compressive strength, f'_c , of 3,000 psi.
- Minimum distance to edge of panel is $2h_{ef}$.

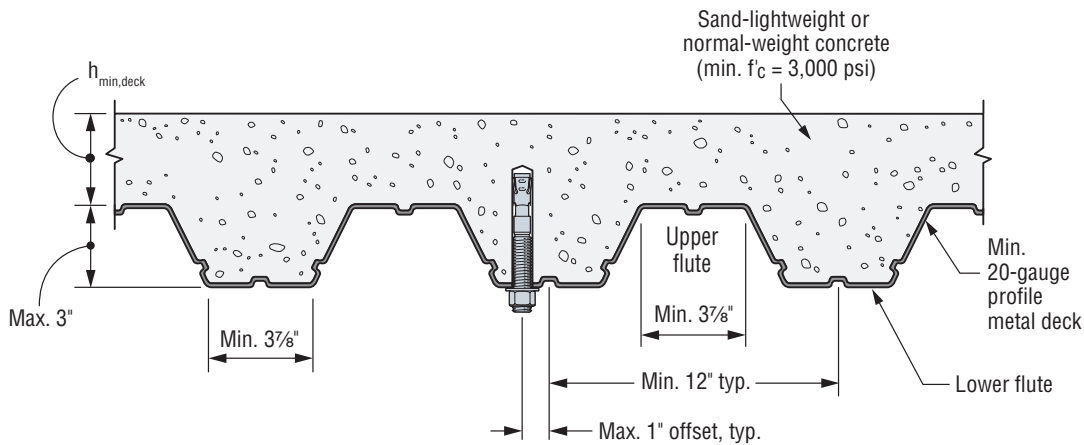
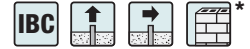


Figure 3

* See p. 13 for an explanation of the load table icons.

Strong-Bolt® 2 Design Information — Masonry

Carbon-Steel Strong-Bolt 2 Tension and Shear Loads in
8" Lightweight, Medium-Weight and Normal-Weight Grout-Filled CMU



Size in. (mm)	Drill Bit Dia. (in.)	Min. Embed. Depth in. (mm)	Install. Torque ft.-lb. (N-m)	Critical Edge Dist. in. (mm)	Critical End Dist. in. (mm)	Critical Spacing in. (mm)	Tension Load		Shear Load	
							Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)
Anchor Installed in the Face of the CMU Wall (See Figure 1)										
1/4 (6.4)	1/4	1 3/4 (45)	4 (5.4)	12 (305)	12 (305)	8 (203)	1,150 (5.1)	230 (1.0)	1,500 (6.7)	300 (1.3)
3/8 (9.5)	3/8	2 7/8 (67)	20 (27.1)	12 (305)	12 (305)	8 (203)	2,185 (9.7)	435 (1.9)	3,875 (17.2)	775 (3.4)
1/2 (12.7)	1/2	3 1/2 (89)	35 (47.5)	12 (305)	12 (305)	8 (203)	2,645 (11.8)	530 (2.4)	5,055 (22.5)	1,010 (4.5)
5/8 (15.9)	5/8	4 3/8 (111)	55 (74.6)	20 (508)	20 (508)	8 (203)	4,460 (19.8)	890 (4.0)	8,815 (39.2)	1,765 (7.9)
3/4 (19.1)	3/4	5 1/4 (133)	100 (135.6)	20 (508)	20 (508)	8 (203)	5,240 (23.3)	1,050 (4.7)	12,450 (55.4)	2,490 (11.1)

- The tabulated allowable loads are based on a safety factor of 5.0 for installation under the IBC and IRC.
- Listed loads may be applied to installations on the face of the CMU wall at least 1 1/4" away from headjoints.
- Values for 8"-wide concrete masonry units (CMU) with a minimum specified compressive strength of masonry, f'_m , at 28 days is 1,500 psi.
- Embedment depth is measured from the outside face of the concrete masonry unit.
- Tension and shear loads may be combined using the parabolic interaction equation ($n = 5/8$).
- Refer to allowable load adjustment factors for edge distance and spacing on p. 146.
- Allowable loads may be increased 33 1/3% for short-term loading due to wind forces or seismic forces where permitted by code.

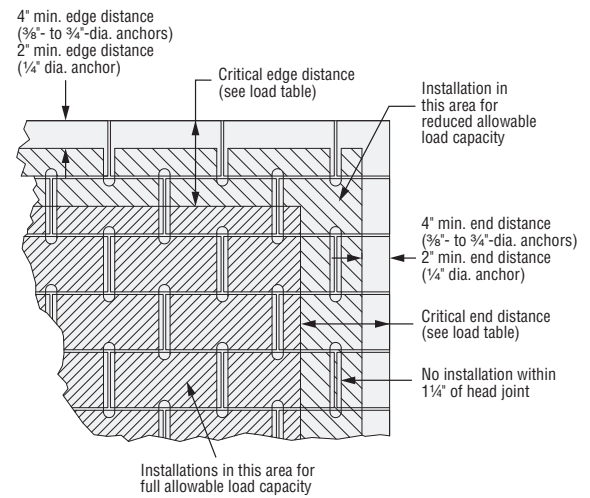


Figure 1

Carbon-Steel Strong-Bolt 2 Tension and Shear Loads in
8" Lightweight, Medium-weight and Normal-Weight Grout-Filled CMU



Size in. (mm)	Drill Bit Dia. in.	Min. Embed. Depth in. (mm)	Install. Torque ft.-lb. (N-m)	Min. Edge. Dist. in. (mm)	Critical End Dist. in. (mm)	Critical Spacing in. (mm)	Tension Load		Shear Load Perp. To Edge		Shear Load Parallel To Edge	
							Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)	Ultimate lb. (kN)	Allowable lb. (kN)
Anchor Installed in Cell Opening or Web (Top of Wall) (See Figure 2)												
1/2 (12.7)	1/2	3 1/2 (89)	35 (47.5)	1 3/4 (45)	12 (305)	8 (203)	2,080 (9.3)	415 (1.8)	1,165 (5.2)	235 (1.0)	3,360 (14.9)	670 (3.0)
5/8 (15.9)	5/8	4 3/8 (111)	55 (74.6)	1 3/4 (45)	12 (305)	8 (203)	3,200 (14.2)	640 (2.8)	1,370 (6.1)	275 (1.2)	3,845 (17.1)	770 (3.4)

- The tabulated allowable loads are based on a safety factor of 5.0 for installation under the IBC and IRC.
- Values for 8"-wide concrete masonry units (CMU) with a minimum specified compressive strength of masonry, f'_m , at 28 days is 1,500 psi.
- Tension and shear loads may be combined using the parabolic interaction equation ($n = 5/8$).
- Refer to allowable load adjustment factors for edge distance and spacing on p. 146.
- Allowable loads may be increased 33 1/3% for short-term loading due to wind forces or seismic forces where permitted by code.

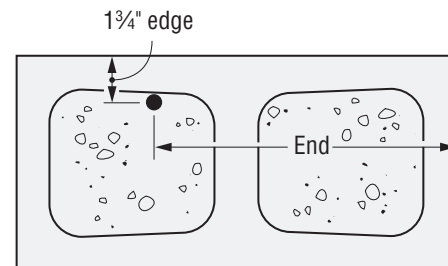


Figure 2

* See p. 13 for an explanation of the load table icons.

Strong-Bolt® 2 Design Information — Masonry

Carbon-Steel Strong-Bolt 2 Allowable Load Adjustment Factors for Face-of-Wall Installation in 8" Grout-Filled CMU: Edge Distance and Spacing, Tension and Shear Loads

How to use these charts:

1. The following tables are for reduced edge distance and spacing.
2. Locate the anchor size to be used for either a tension and/or shear load application.
3. Locate the embedment (E) at which the anchor is to be installed.
4. Locate the edge distance (c_{act}) or spacing (s_{act}) at which the anchor is to be installed.
5. The load adjustment factor (f_c or f_s) is the intersection of the row and column.
6. Multiply the allowable load by the applicable load adjustment factor.
7. Reduction factors for multiple edges or spacings are multiplied together.

Edge or End Distance Tension (f_c)

c_{act} (in.)	Dia.	1/4	3/8	1/2	5/8	3/4	IBC*
	E	1 3/4	2 5/8	3 1/2	4 3/8	5 1/4	
	c_{cr}	12	12	12	20	20	
	c_{min}	2	4	4	4	4	
	f_{cmin}	1.00	1.00	1.00	1.00	0.97	
2		1.00					
4		1.00	1.00	1.00	1.00	0.97	
6		1.00	1.00	1.00	1.00	0.97	
8		1.00	1.00	1.00	1.00	0.98	
10		1.00	1.00	1.00	1.00	0.98	
12		1.00	1.00	1.00	1.00	0.99	
14					1.00	0.99	
16					1.00	0.99	
18					1.00	1.00	
20					1.00	1.00	

Edge or End Distance Shear (f_c)

c_{act} (in.)	Dia.	1/4	3/8	1/2	5/8	3/4	IBC*
	E	1 3/4	2 5/8	3 1/2	4 3/8	5 1/4	
	c_{cr}	12	12	12	20	20	
	c_{min}	2	4	4	4	4	
	f_{cmin}	0.88	0.71	0.60	0.36	0.28	
2		0.88					
4		0.90	0.71	0.60	0.36	0.28	
6		0.93	0.78	0.70	0.44	0.37	
8		0.95	0.86	0.80	0.52	0.46	
10		0.98	0.93	0.90	0.60	0.55	
12		1.00	1.00	1.00	0.68	0.64	
14					0.76	0.73	
16					0.84	0.82	
18					0.92	0.91	
20					1.00	1.00	

Spacing Tension (f_s)

s_{act} (in.)	Dia.	1/4	3/8	1/2	5/8	3/4	IBC*
	E	1 3/4	2 5/8	3 1/2	4 3/8	5 1/4	
	s_{cr}	8	8	8	8	8	
	s_{min}	4	4	4	4	4	
	f_{smin}	1.00	1.00	0.93	0.86	0.80	
4		1.00	1.00	0.93	0.86	0.80	
6		1.00	1.00	0.97	0.93	0.90	
8		1.00	1.00	1.00	1.00	1.00	

Spacing Shear (f_s)

s_{act} (in.)	Dia.	1/4	3/8	1/2	5/8	3/4	IBC*
	E	1 3/4	2 5/8	3 1/2	4 3/8	5 1/4	
	s_{cr}	8	8	8	8	8	
	s_{min}	4	4	4	4	4	
	f_{smin}	1.00	1.00	1.00	1.00	1.00	
4		1.00	1.00	1.00	1.00	1.00	
6		1.00	1.00	1.00	1.00	1.00	
8		1.00	1.00	1.00	1.00	1.00	

Load Adjustment Factors for Carbon-Steel Strong-Bolt 2 Wedge Anchors in Top-of-Wall Installation in 8" Grout-Filled CMU: Edge Distance and Spacing, Tension and Shear Loads

End Distance Tension (f_c)

s_{act} (in.)	Dia.	1/2	5/8	IBC*
	E	3 1/2	4 3/8	
	c_{cr}	12	12	
	c_{min}	4	4	
	f_{cmin}	1.00	1.00	
4		1.00	1.00	
6		1.00	1.00	
8		1.00	1.00	
10		1.00	1.00	
12		1.00	1.00	

End Distance Shear Perpendicular to Edge (f_c)

c_{act} (in.)	Dia.	1/2	5/8	IBC*
	E	3 1/2	4 3/8	
	c_{cr}	12	12	
	c_{min}	4	4	
	f_{cmin}	0.90	0.83	
4		0.90	0.83	
6		0.93	0.87	
8		0.95	0.92	
10		0.98	0.96	
12		1.00	1.00	

End Distance Shear Parallel to Edge (f_c)

c_{act} (in.)	Dia.	1/2	5/8	IBC*
	E	3 1/2	4 3/8	
	c_{cr}	12	12	
	c_{min}	4	4	
	f_{cmin}	0.53	0.50	
4		0.53	0.50	
6		0.65	0.63	
8		0.77	0.75	
10		0.88	0.88	
12		1.00	1.00	

Spacing Tension (f_s)

s_{act} (in.)	Dia.	1/2	5/8	IBC*
	E	3 1/2	4 3/8	
	s_{cr}	8	8	
	s_{min}	4	4	
	f_{smin}	0.93	0.86	
4		0.93	0.86	
6		0.97	0.93	
8		1.00	1.00	

Spacing Shear Perpendicular to Edge or Parallel to Edge (f_s)

s_{act} (in.)	Dia.	1/2	5/8	IBC*
	E	3 1/2	4 3/8	
	s_{cr}	8	8	
	s_{min}	4	4	
	f_{smin}	1.00	1.00	
4		1.00	1.00	
6		1.00	1.00	
8		1.00	1.00	

* See p. 13 for an explanation of the load table icons.